



# Analysis and Modeling of Skywave Behavior



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Technical Symposium of the International Loran Association  
October 13-15, 2009  
Portland, ME

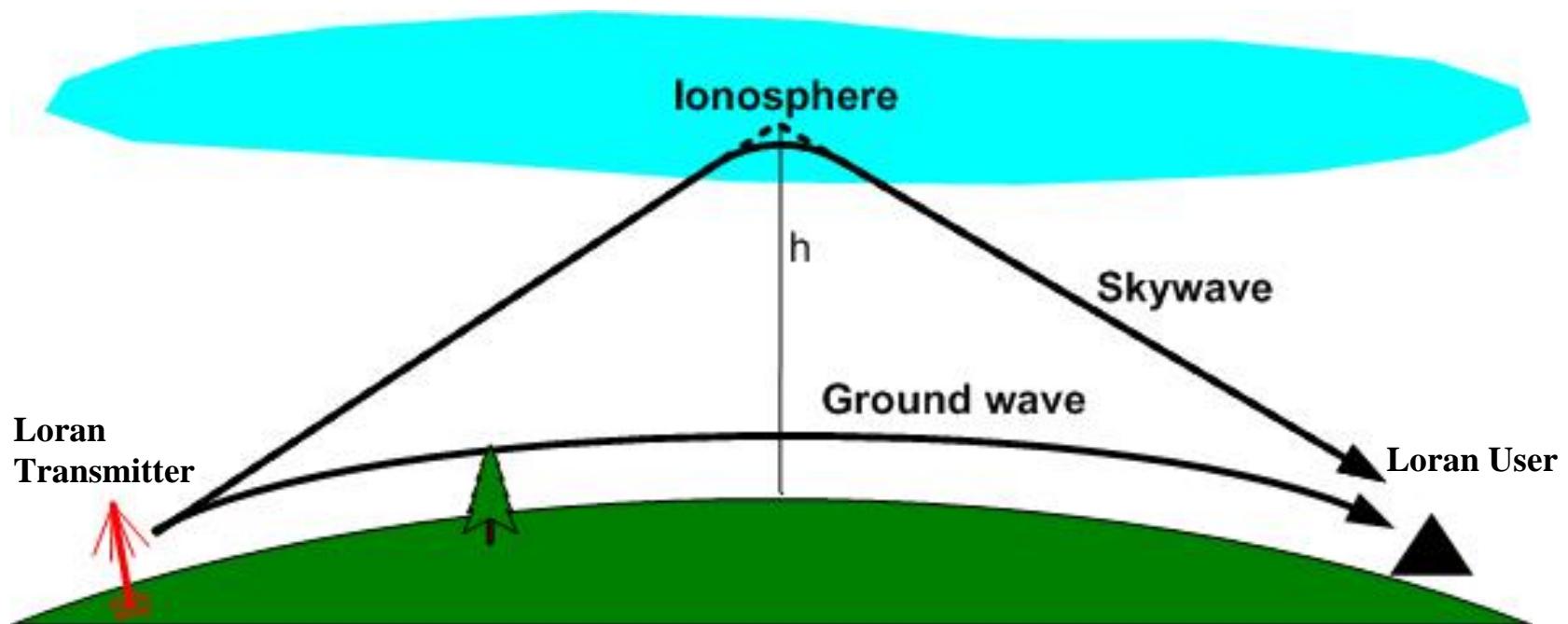


# Outline

- Skywave and Early Skywave
  - Utility of characterizing skywave for detection
- Modeling Skywave (delay, strength)
  - Effects of Filtering
  - Modeling & Results
  - Phase reversal & skywave ECD



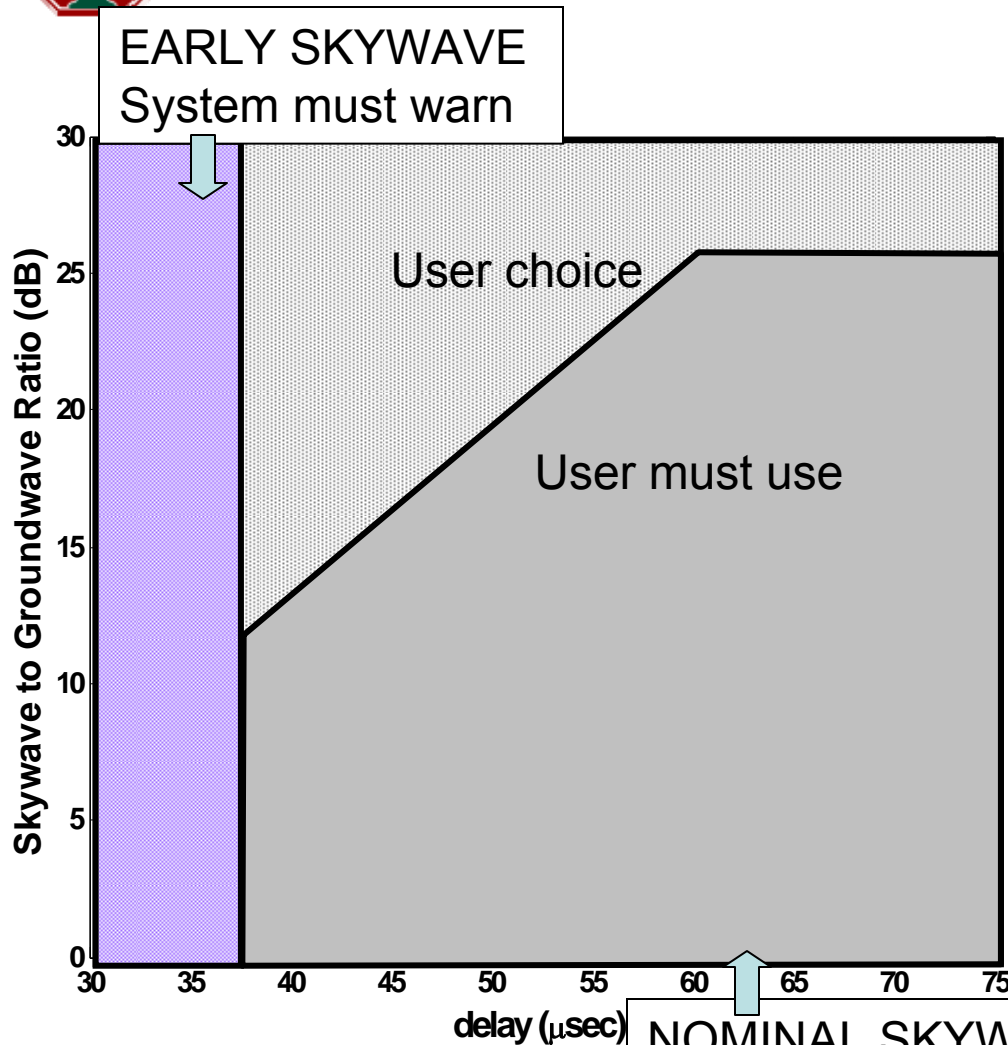
# Skywave



*Single hop skywave is shown*



# Early Skywave

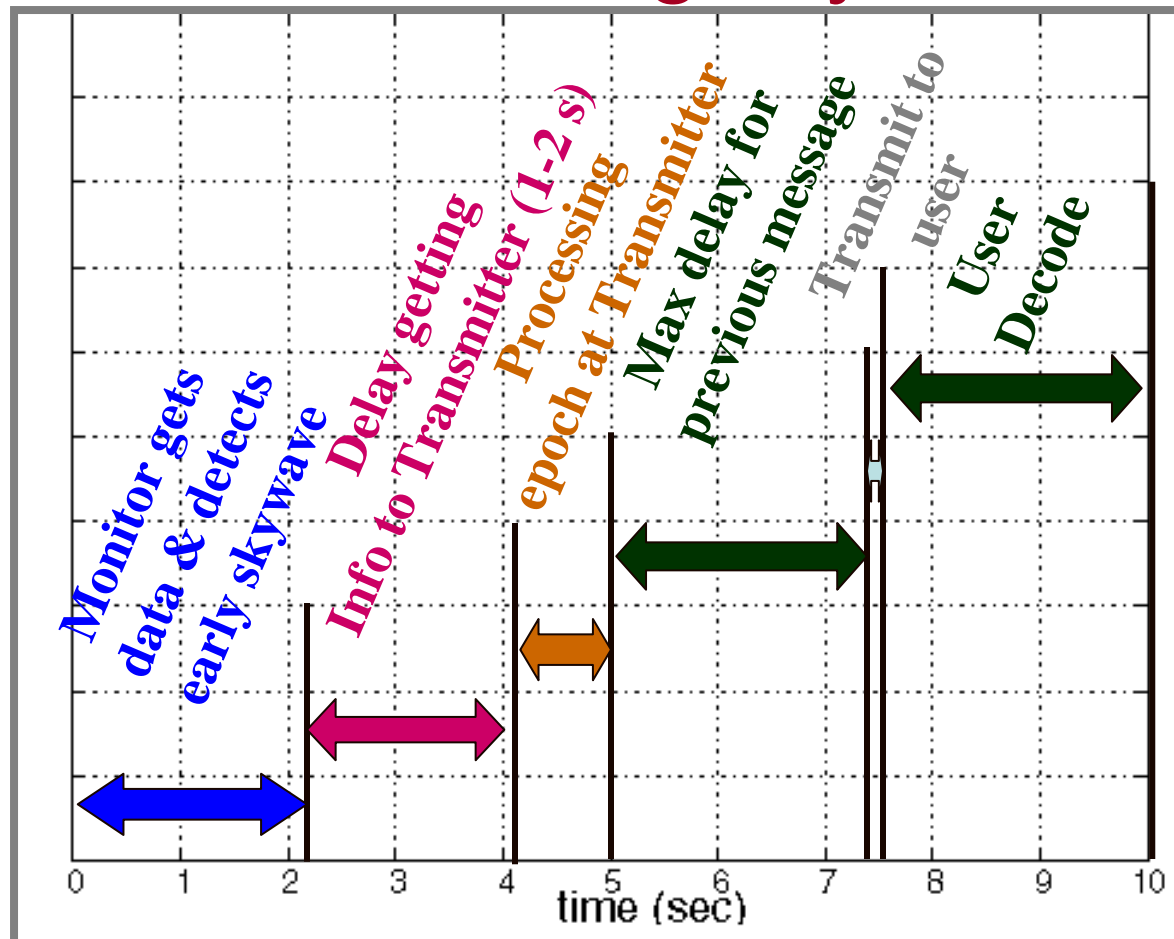


- Early skywave has smaller delay than typical
  - More adverse effect on receiver
  - Harder to detect
- Aviation & maritime specifications have used 35 & 37.5 μs as demarcation line
- System should provide warning
  - Network based solution reduces missed detection
  - Skywave modeling to aid TTA

NOMINAL SKYWAVE  
User responsible for mitigating



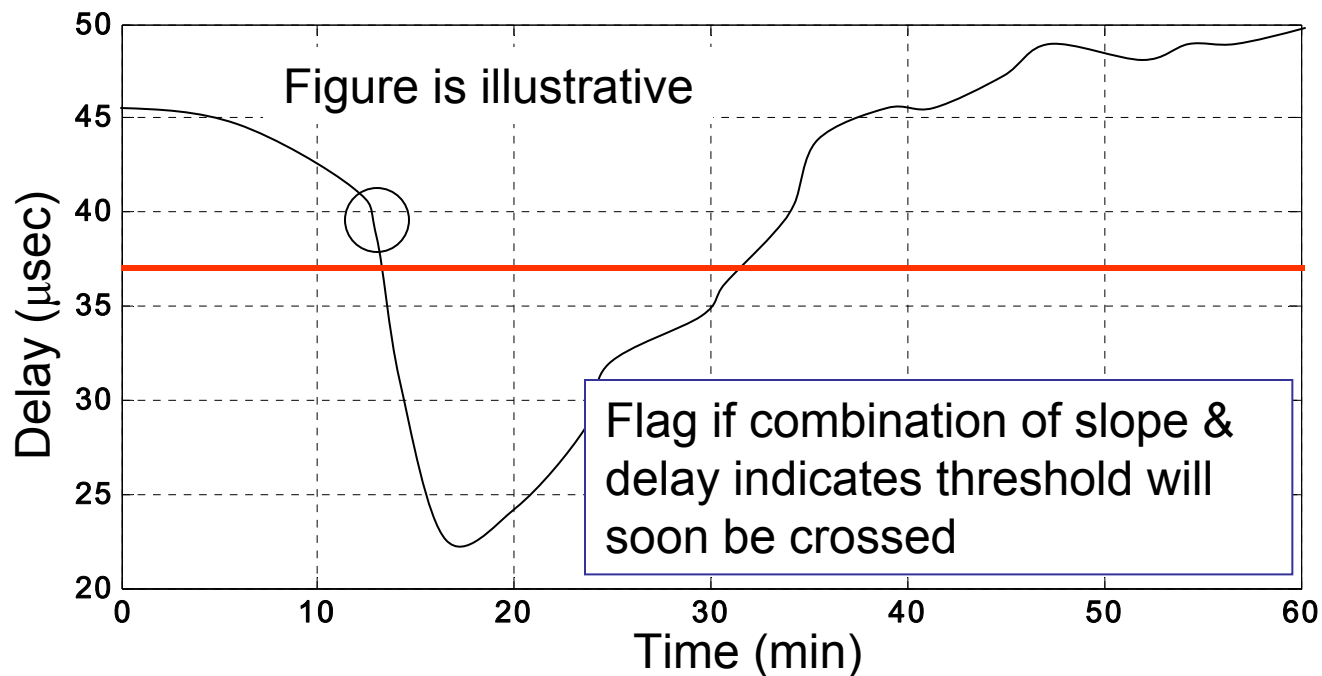
# Time To Alert & Need for understanding skywave



- Meeting 10 sec TTA means detection within a few seconds
- Even a 60 sec TTA means detection in ~ 50 seconds



# Example of Use for Detection



- Detection enabled by accurately estimating delay
  - Can use delay estimate to determine progression of skywave event
  - Example: Use delay and delay rate to “predict” onset of early skywave
- Need to understand skywave well for estimation



# Estimating Skywave

- Determine the skywave properties
  - Delay, Skywave/Groundwave Ratio (SGR)
  - Rates of change
- Two sources of data from GRI 9940
  - US Coast Guard SAM data (“out”)
  - Enhanced Loran Receiver (ELR)
- First need model for skywave
  - Also filter effects



# Basic Skywave Model

$$g(t) = A_g (t - \tau_g)^2 e^{\left(\frac{-2(t - \tau_g)}{65 \mu\text{sec}}\right)} \sin\left(\frac{2\pi t}{10 \mu\text{sec}}\right)$$
$$g(t) = B_g(t) \sin\left(\frac{2\pi t}{10 \mu\text{sec}}\right)$$

$$s(t) = \text{sign}_s A_s (t - \tau_s - d)^2 e^{\left(\frac{-2(t - \tau_s - d)}{65 \mu\text{sec}}\right)} \sin\left(\frac{2\pi(t - d)}{10 \mu\text{sec}}\right)$$
$$s(t) = \text{sign}_s B_s(t) \sin\left(\frac{2\pi(t - d)}{10 \mu\text{sec}}\right)$$

$$c(t) = B_g(t) \sin\left(\frac{2\pi t}{10 \mu\text{sec}}\right) + \text{sign}_s B_s(t) \sin\left(\frac{2\pi(t - d)}{10 \mu\text{sec}}\right)$$

- Model based on standard Loran signal definition
  - Generalize envelope
- Skywave is replica of groundwave with few differences
  - ECD, phase code, amplitude, delay
- Form composite model



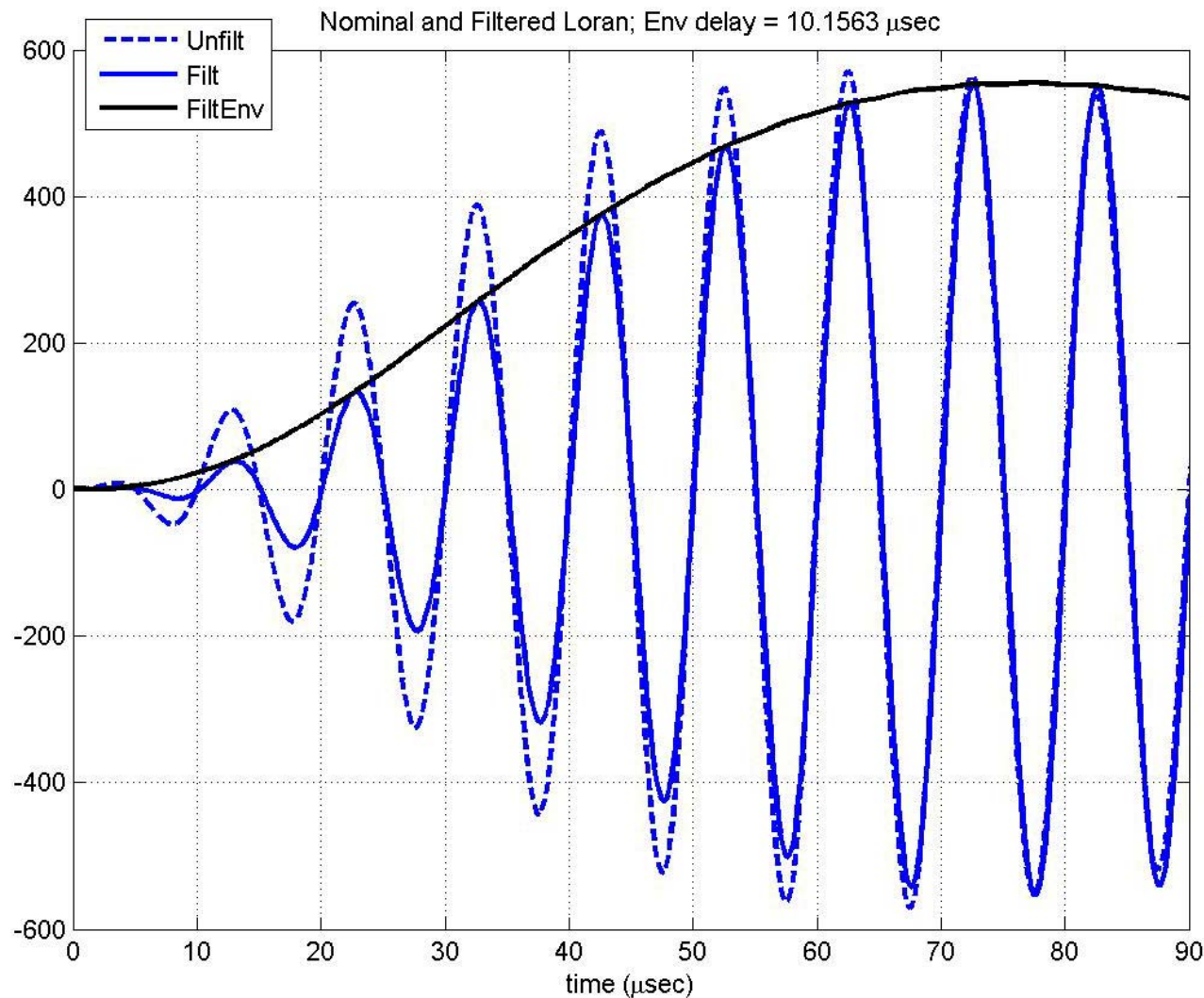


# Preliminary analysis

- Use USCG “out” data (Locus LRS IIID)
  - Provides TDOA and ECD
- Assumptions
  - Filter: 2<sup>nd</sup> order Butterworth
  - Skywave ECD can be different from groundwave
  - Skywave is phase reverse from groundwave
  - No other attempt was made to replicate LRSIIID performance
    - ECD is calculated using the ratio of the envelope at 17.5 to 22.5  $\mu$ sec and extrapolated
- Next 4 slides show the effects of skywave given the filter assumptions



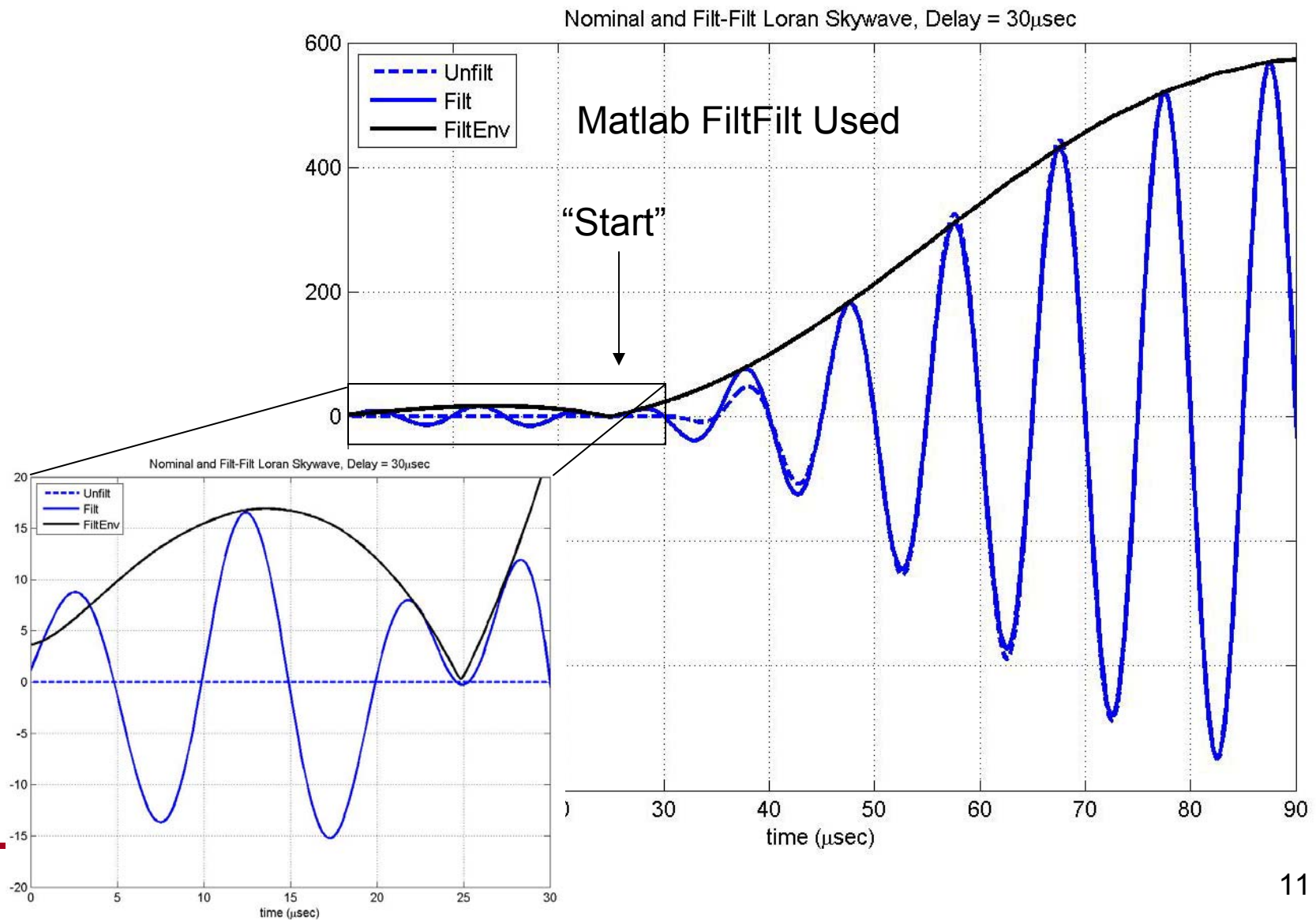
# Explained: Butterworth Filter



- 2<sup>nd</sup> order Butterworth filter
- Envelope peak delayed  $\sim 12.5 \mu\text{sec}$
- Carrier is visible after  $5 \mu\text{sec}$
- Skywave effect greater & earlier than without filter
  - 35  $\mu\text{sec}$  delay can effect 30  $\mu\text{sec}$  tracking point

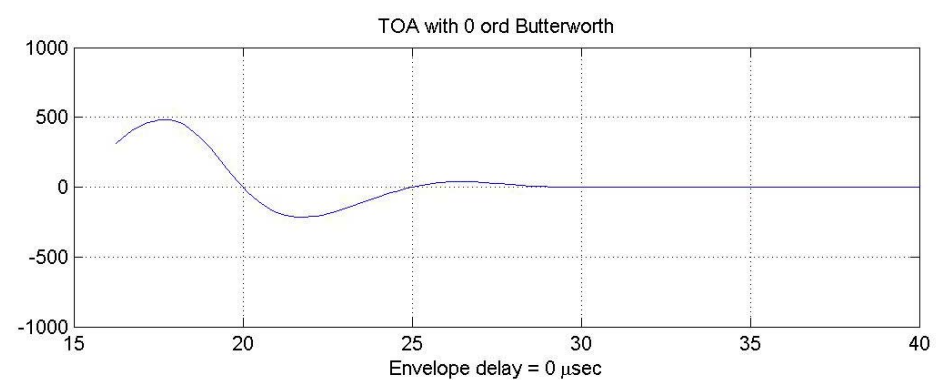
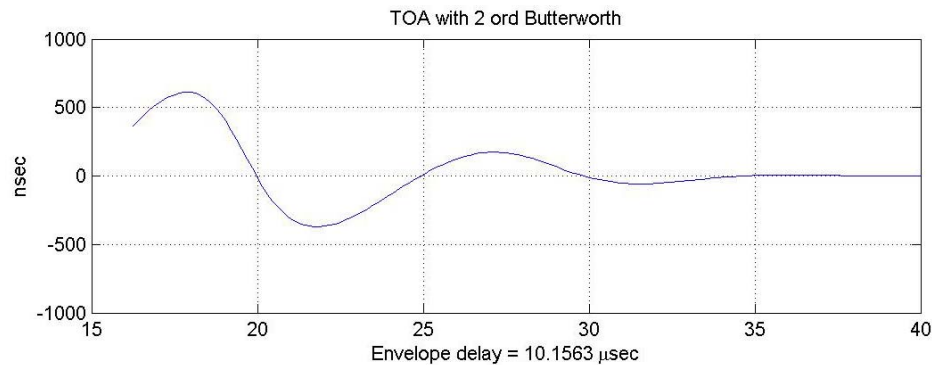
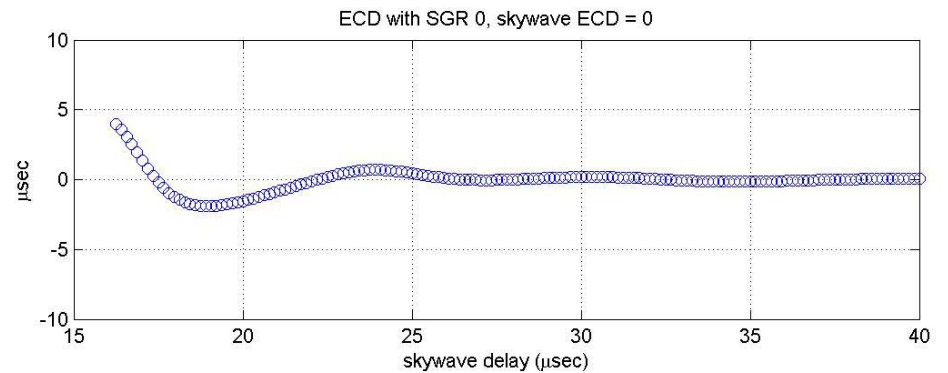
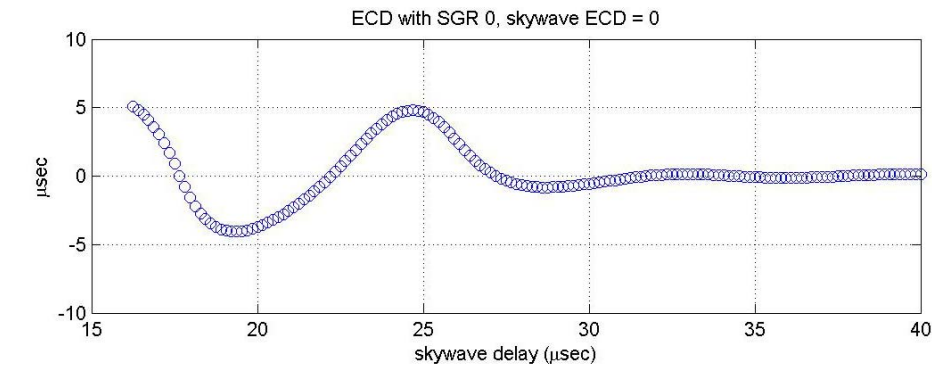


# Explained: Non-causal Butterworth





# Skywave Effects: Filtered vs Unfiltered



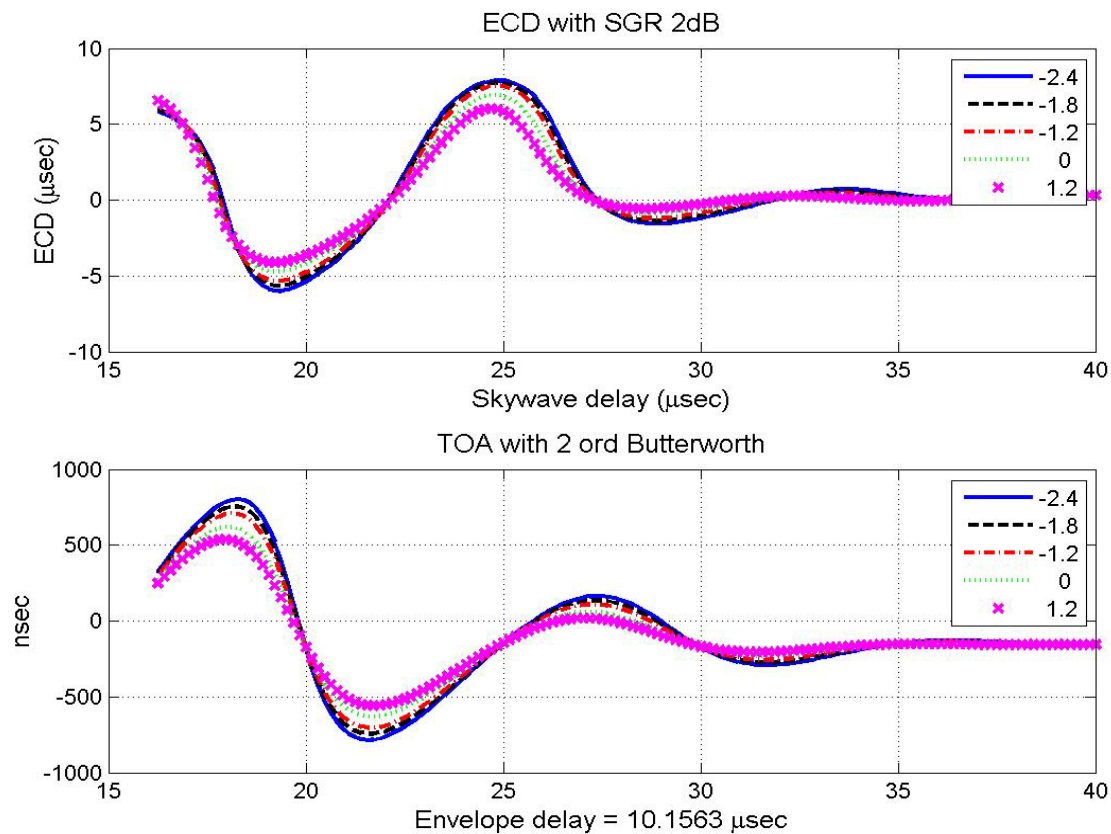
2<sup>nd</sup> Order Butterworth Filter

No Filter

Filtering amplifies affect of skywave and results in skywave affect happening earlier



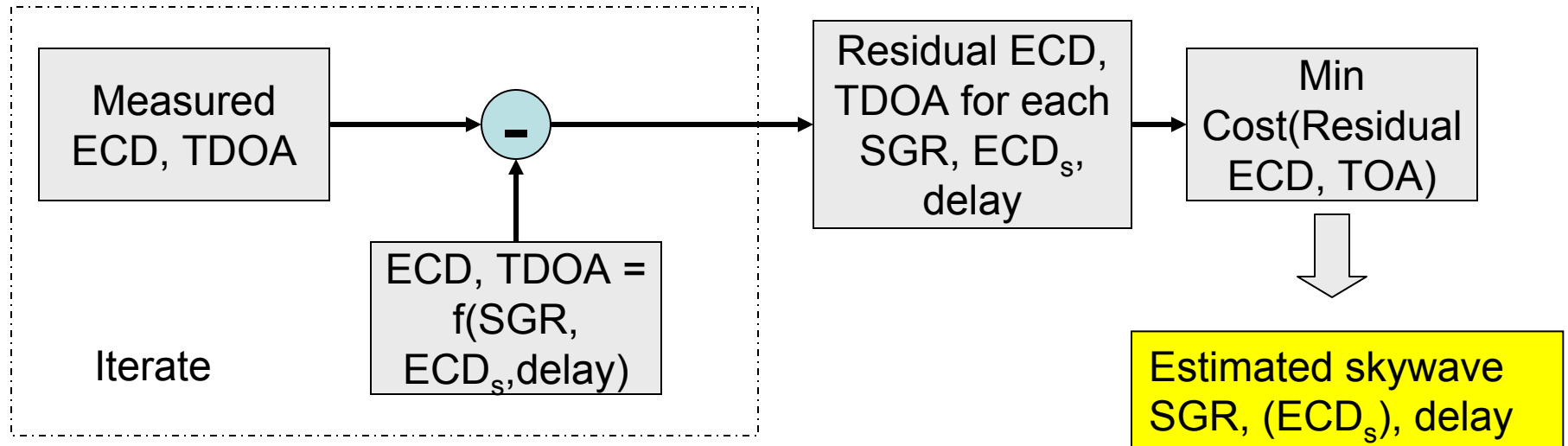
# Skywave Effect Curves



- Curves of TOA (TDOA), ECD variations due to SGR, ECD as a function of delay



# Determining delay and SGR



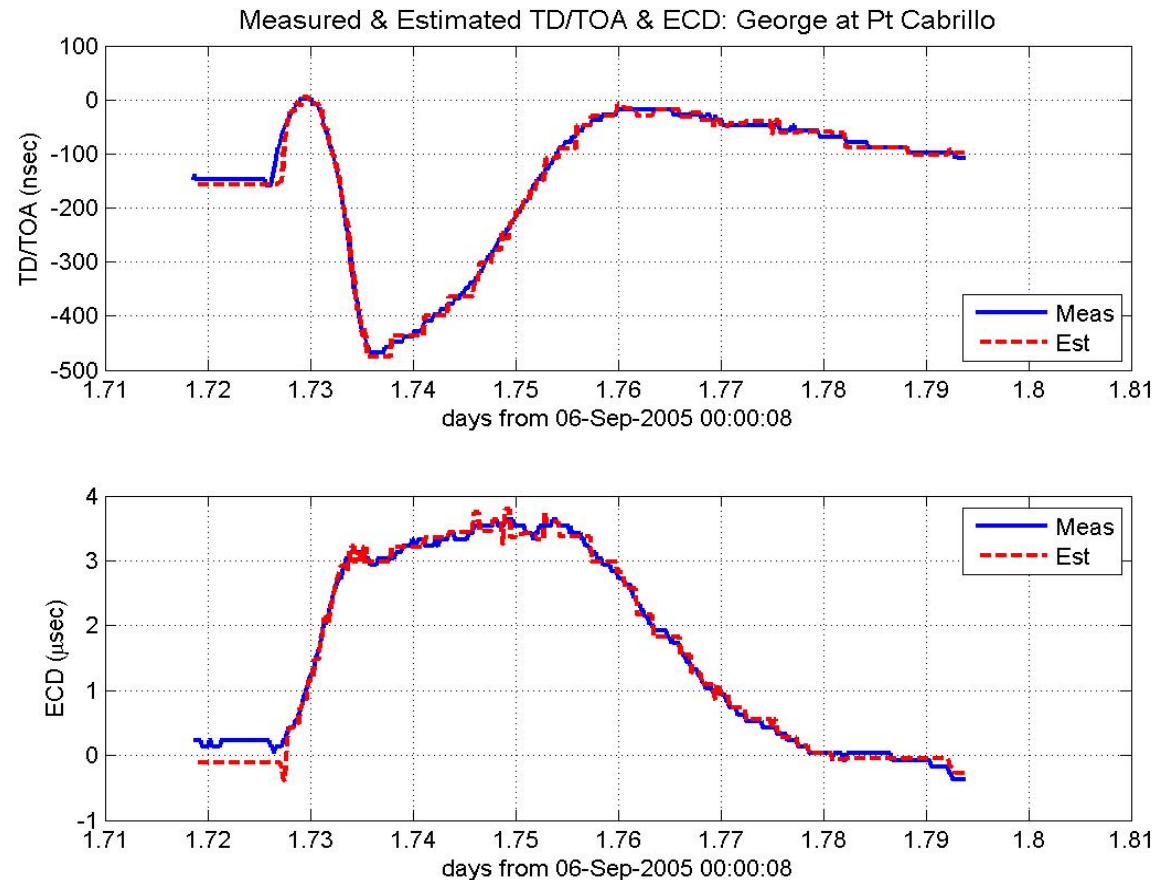
- Minimize sum of residual ECD & TOA
- Estimation is made “ad hoc”
  - No interpolation (SGR quantization  $\geq 0.5$  dB)
  - Cost function based on roughly equal weighting of ECD, TD, delay change
- Results seems to reasonably replicate
  - Is it just curve fitting or is the physics right?





# Measured & Estimate Derived TD & ECD at George at Pt. Cabrillo Sept 7, 2005

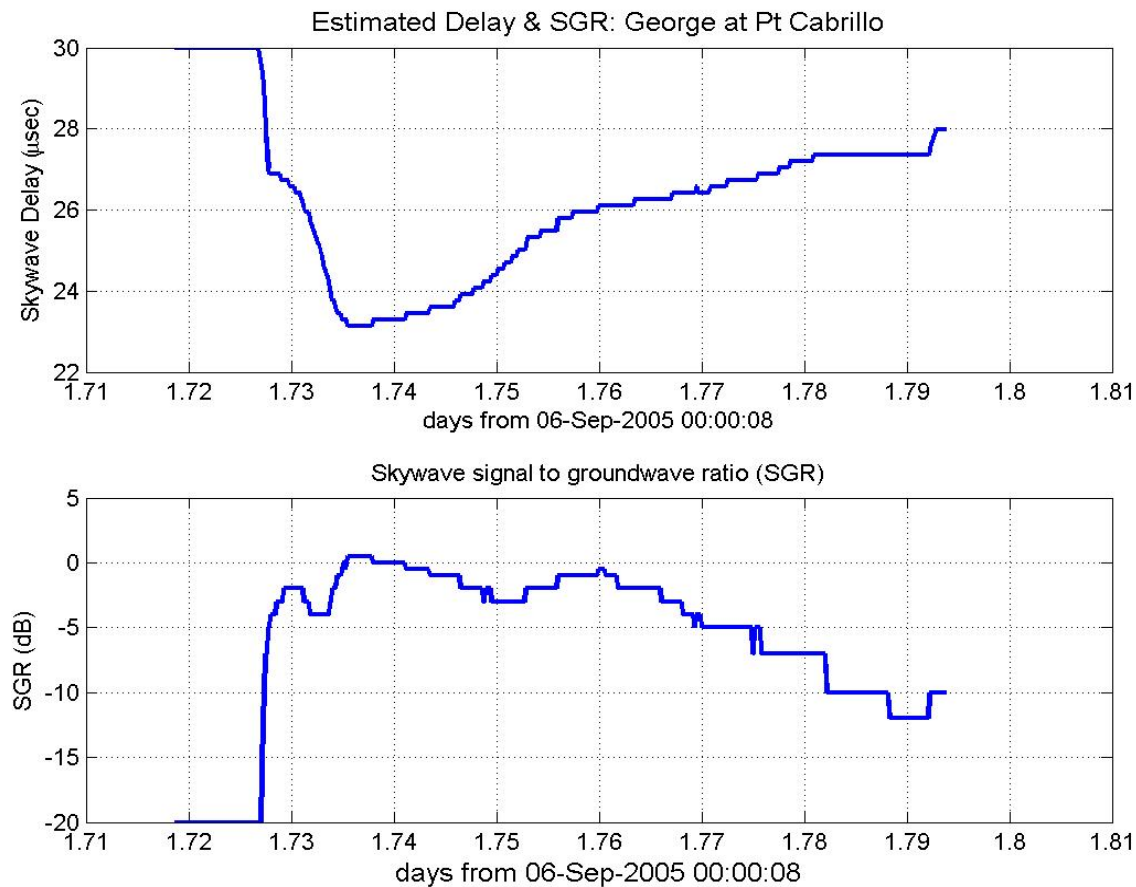
Phase Reversed



Baseline ~ 1020 km



# Estimated Parameters at George at Pt. Cabrillo Sept 7, 2005

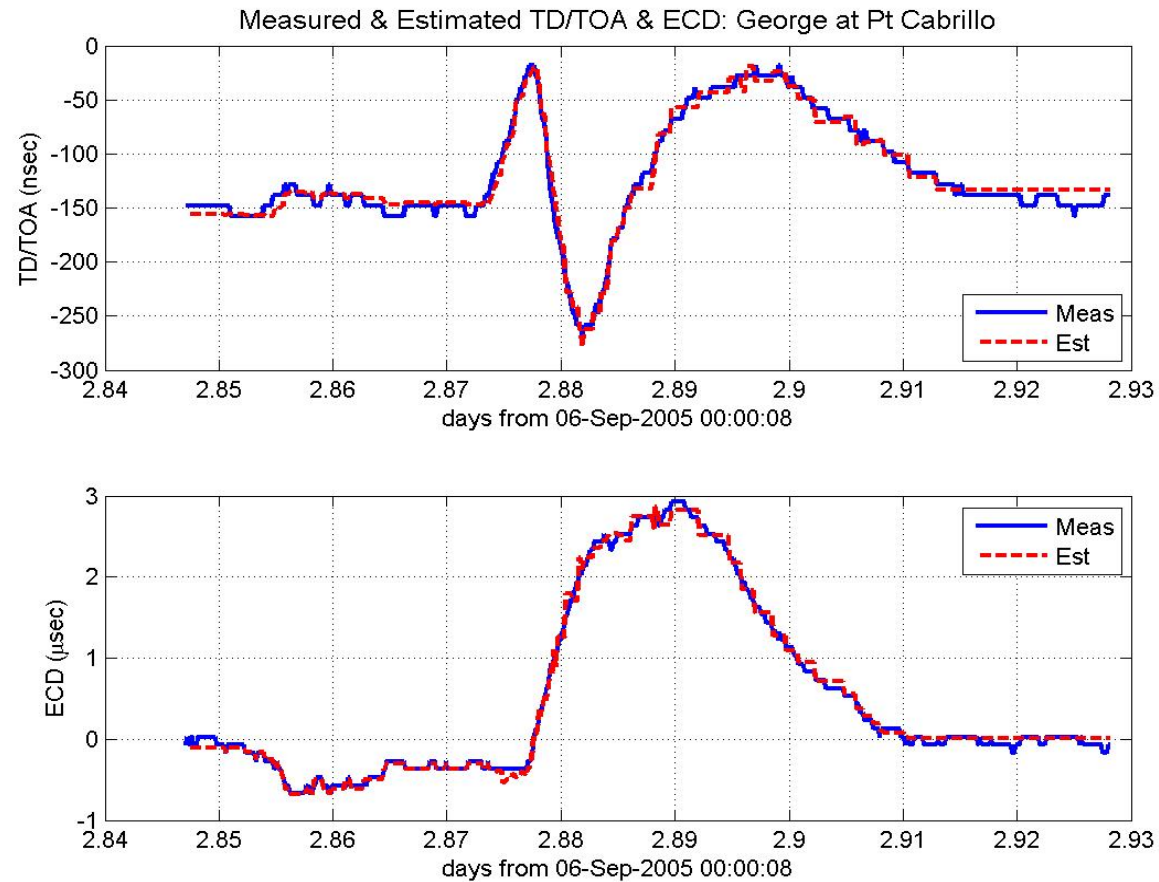






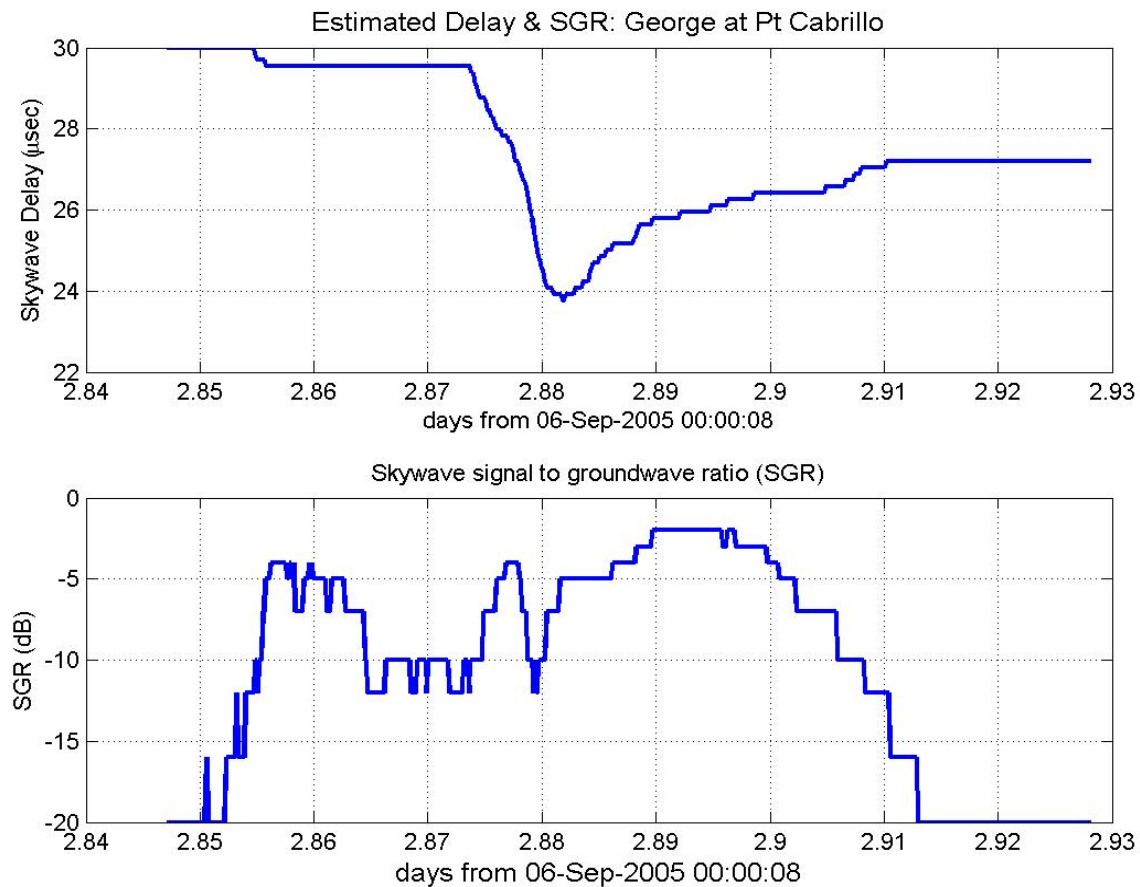
# Measured & Estimate Derived TD & ECD at George at Pt. Cabrillo Sept 8, 2005

Phase Reversed





# Estimated Parameters at George at Pt. Cabrillo Sept 8, 2005





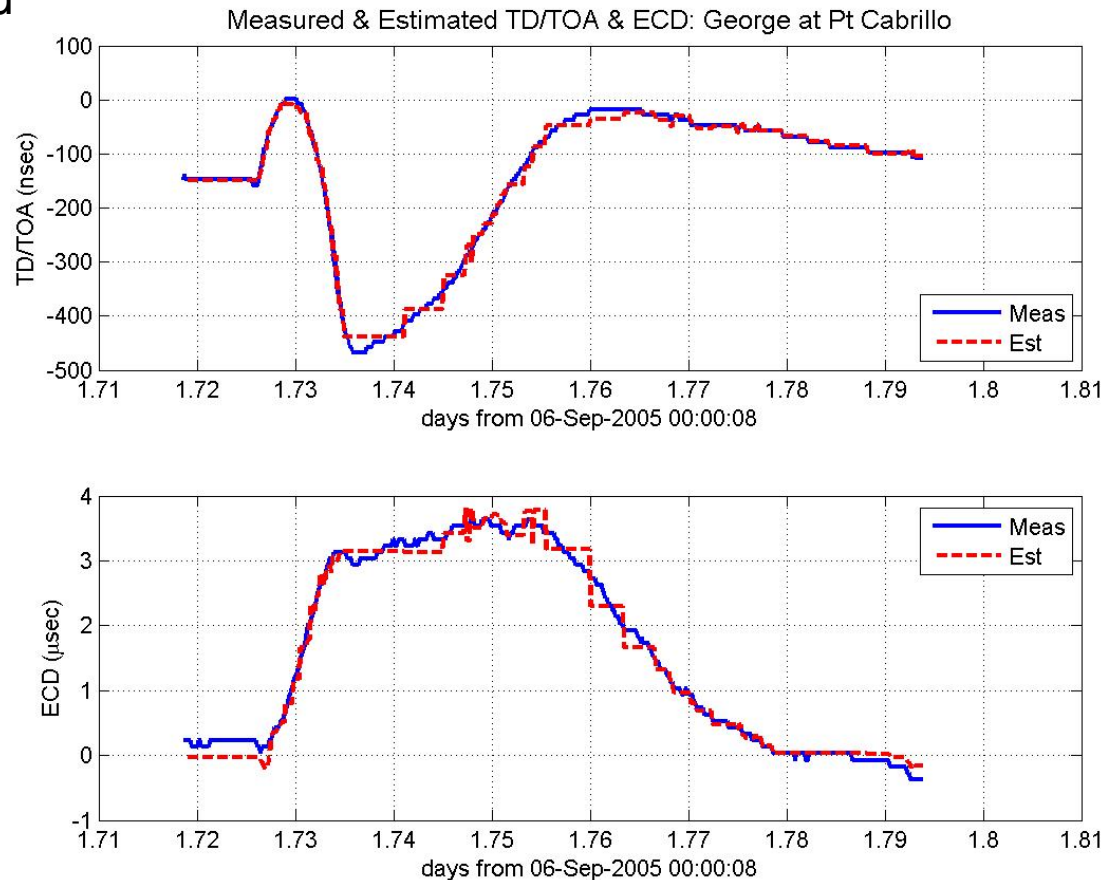
## How do we know that the is correct? Signal Reversal on Skywave?

- Test model with no sign reversal (phase unchanged) on USCG data
  - Data reasonably well model
  - Implied differences from phase reversed (higher SGR,  $\sim 5 \mu\text{sec}$ )
- Past data
- Examine reversal/no sign reversal on ELR data



# Measured & Estimate Derived TD & ECD at George at Pt. Cabrillo Sept 7, 2005

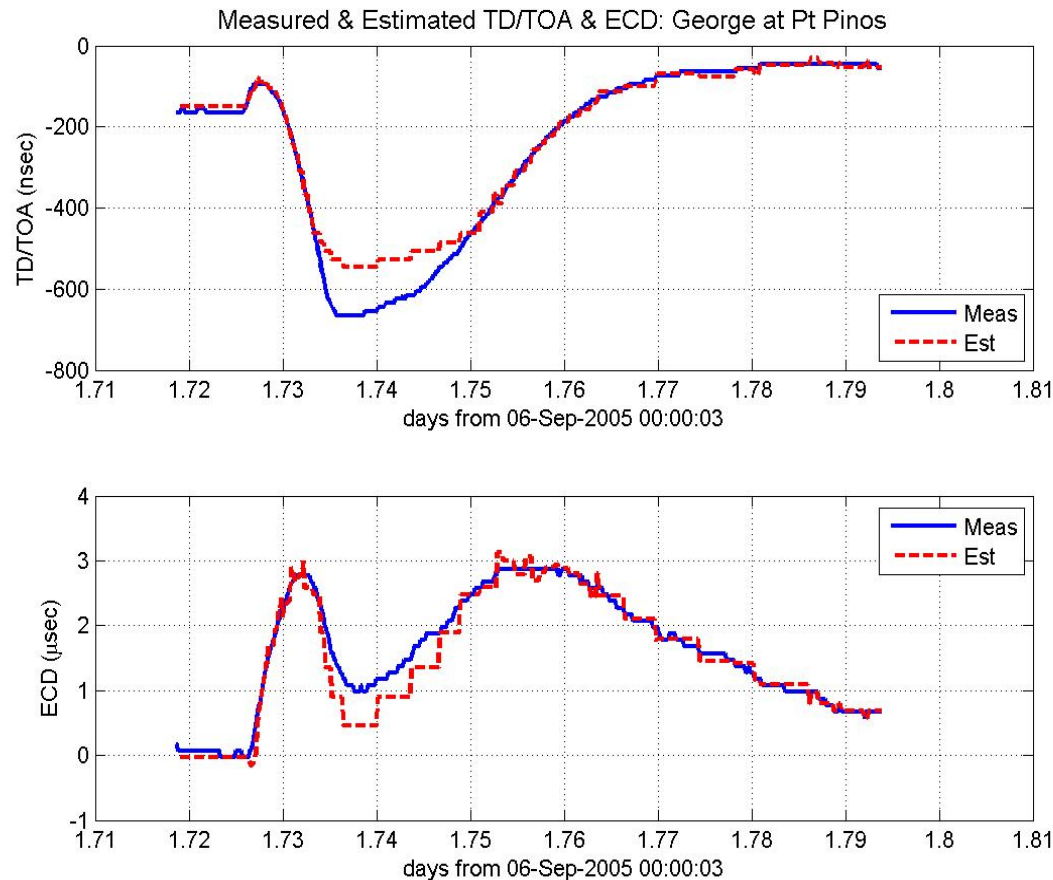
Phase Unchanged





# Measured & Estimate Derived TD & ECD at George at Pt. Pinos Sept 7, 2005

Phase Unchanged

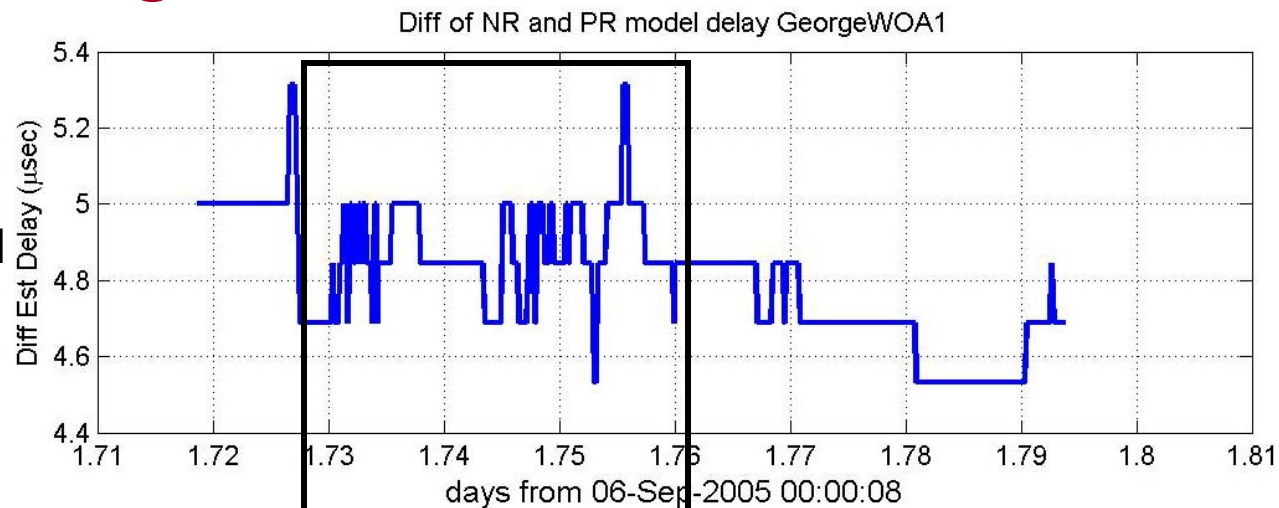


Baseline ~ 1050 km

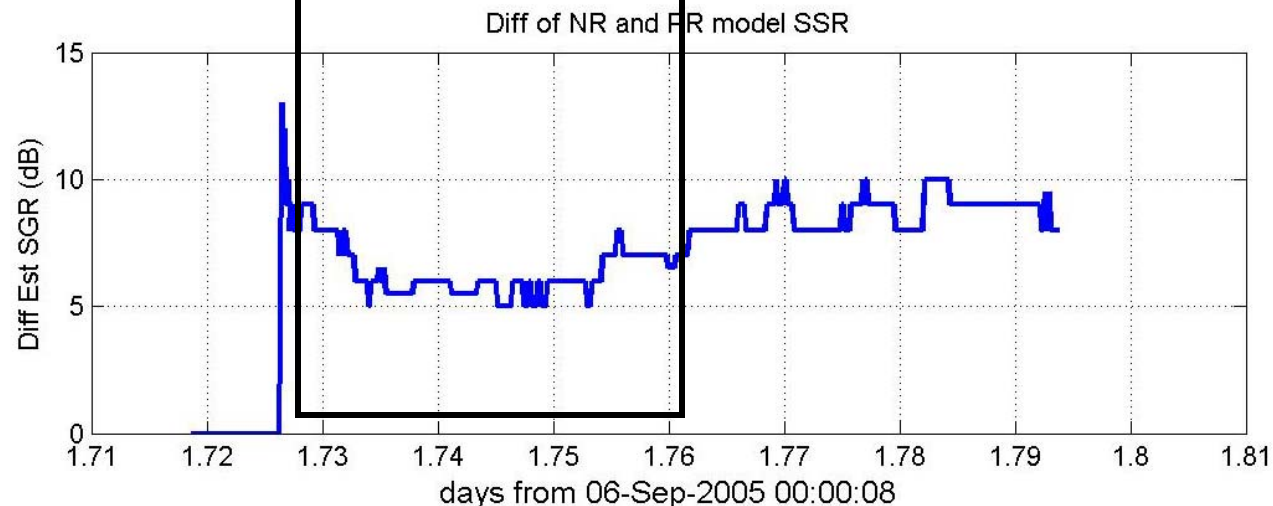


# Difference between Phase Unchanged & Phase Reversed Model

Phase unchanged delay is +5  $\mu\text{sec}$

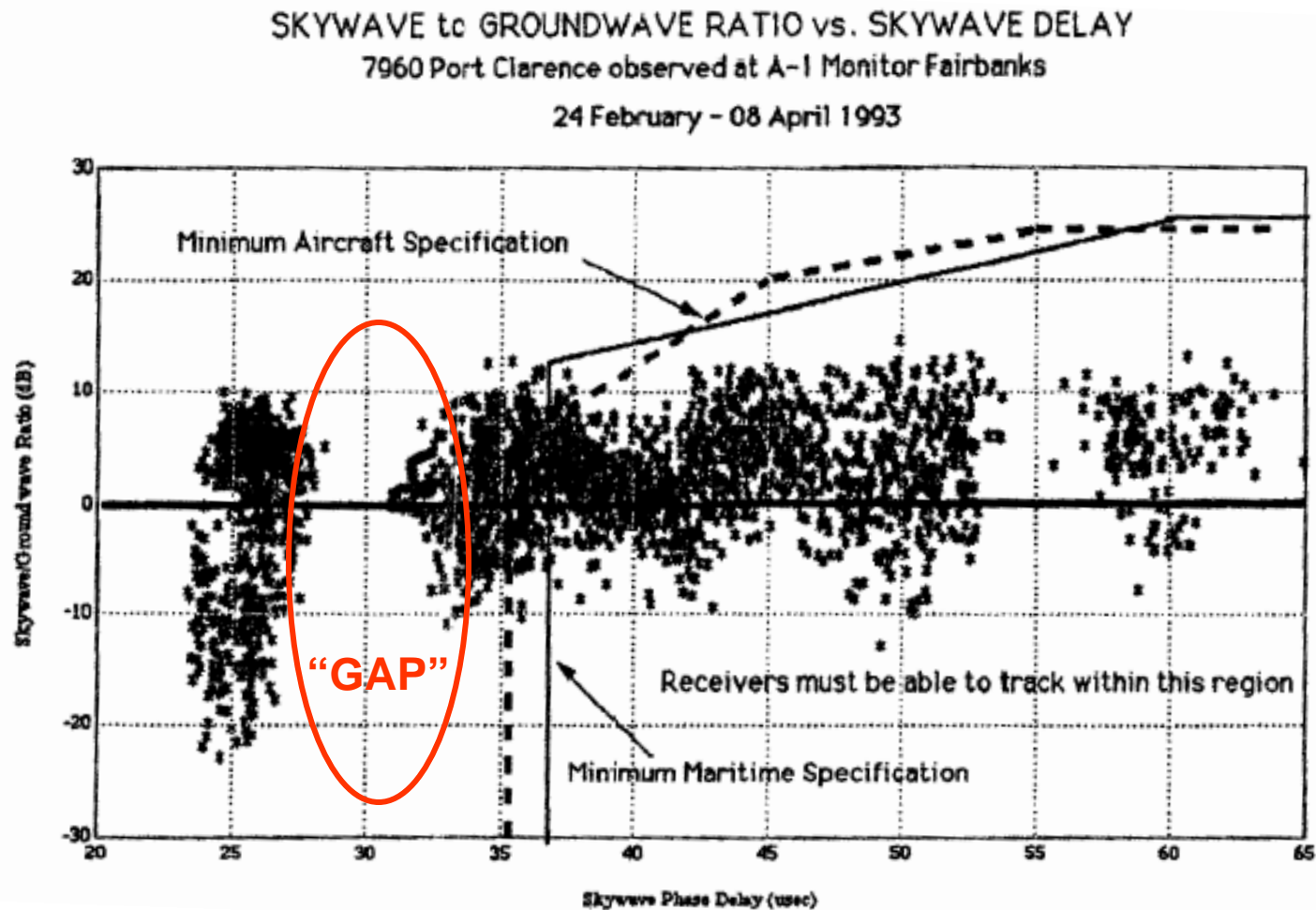


Phase unchanged SGR is 4-10 dB higher





# Phase Reversal in Past Data

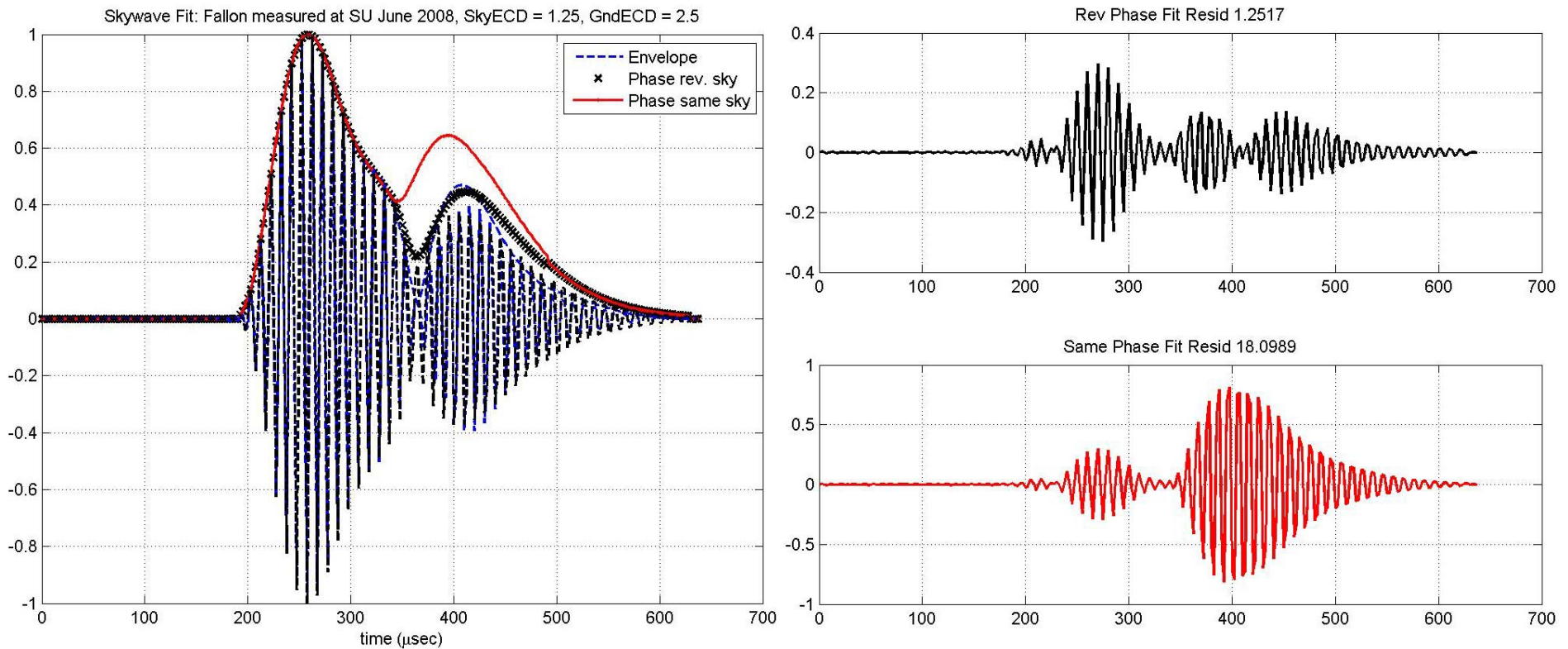


~ 900 km





# Skywave to Groundwave ECD



Skywave ECD is  $\sim -1.25 \mu\text{sec}$  relative to Groundwave  
Values that differs results in larger residuals  
(i.e. 0 or  $\pm 2.5$ ) results in min resid  $\sim 4$





## Summary

- Filter cause skywave to effect signal even if delay  $> 30 \mu\text{sec}$
- Results show that skywave likely has different ECD than groundwave
- Suspect that there is some phase reversal (single hop)



# Acknowledgments & Disclaimer

- The authors gratefully acknowledge the support of the Federal Aviation Administration and Mitchell Narins under Cooperative Agreement 2000-G-028.
- Kirk Montgomery, Benjamin Peterson, and Peter Morris for their help and insight
- The views expressed herein are those of the authors and are not to be construed as official or reflecting the views of the U.S. Coast Guard, Federal Aviation Administration, Department of Transportation or Department of Homeland Security or any other person or organization.